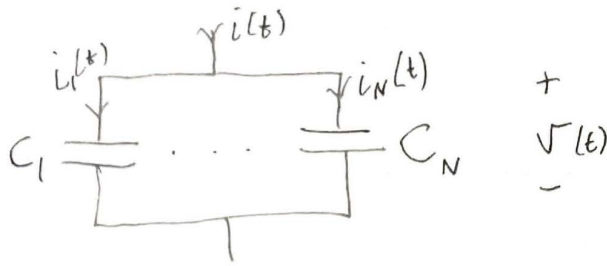


1.



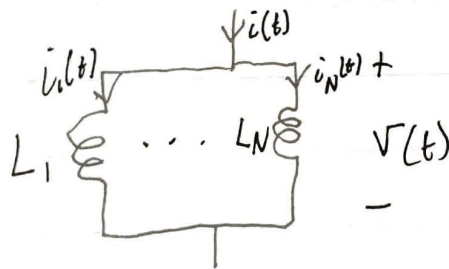
$$i(t) = i_1(t) + \dots + i_N(t)$$

$$C_k \frac{dV}{dt} = i_k, \quad k=1, 2, \dots, N$$

$$\text{So } i(t) = \sum_{k=1}^N i_k = \sum_{k=1}^N C_k \frac{dV}{dt} = \left( \sum_{k=1}^N C_k \right) \frac{dV}{dt} = i(t)$$

$$\text{So } C_{eq} = \sum_{k=1}^N C_k$$

2.



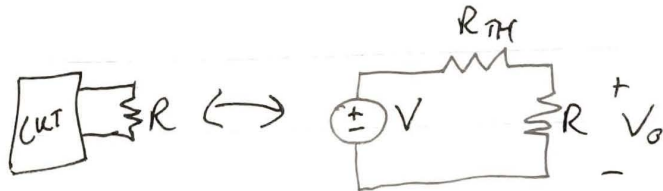

$$i(t) = \sum_{k=1}^N i_k(t), \quad L_k \frac{di_k}{dt} = V(t)$$

$$\frac{di}{dt} = \frac{d}{dt} \sum_{k=1}^N i_k(t) = \sum_{k=1}^N \frac{di_k}{dt} = \frac{V(t)}{L_{eq}} = \sum_{k=1}^N \frac{V(t)}{L_k}$$

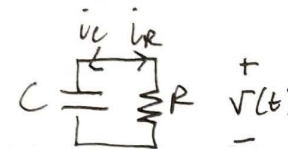
$$\text{So } \frac{1}{L_{eq}} = \sum_{k=1}^N \frac{1}{L_k}$$

or

$$L_{eq} = \frac{1}{\sum_{k=1}^N \frac{1}{L_k}}$$

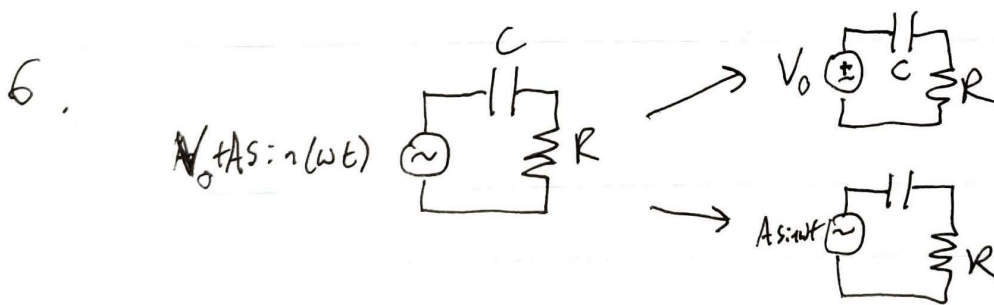
3.  $V_{TH} = V$ ,   $\leftrightarrow$  

$$V_o = V \frac{R}{R + R_{TH}} \Rightarrow R + R_{TH} = \frac{V}{V_o} R \Rightarrow R_{TH} = \left(\frac{V}{V_o} - 1\right) R$$

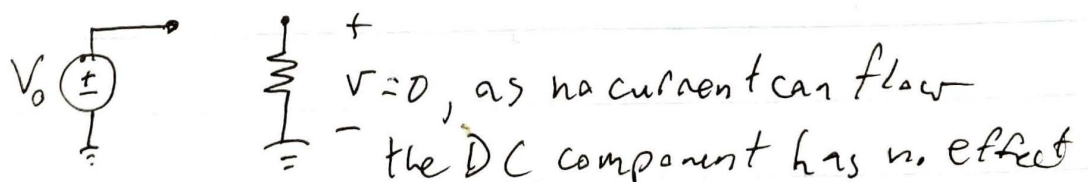
4.   $V(0) = V_o$   $\hookrightarrow$   $i_R = -i_C$   
 $\hookrightarrow \frac{v(t)}{R} = -C \frac{dv}{dt}$

So  $-\frac{dt}{RC} = \frac{dv}{v(t)} \Rightarrow A e^{-t/RC} = v(t)$ ,  $v(0) = A = V_o$  so  
 $v(t) = V_o e^{-t/RC}$

5. As  $C$  grows large  $i(t) = C \frac{dv}{dt} \Rightarrow \frac{dv}{dt} = \frac{i(t)}{C} \approx 0$ , so  
 for short time intervals  $\frac{dv}{dt} \approx 0 \Rightarrow v \approx \text{constant}$  or:  
Capacitor acts as a voltage source



7. At DC,  $C \rightarrow \infty, C$ . so



"The capacitor removes the DC component from the resistor's output"

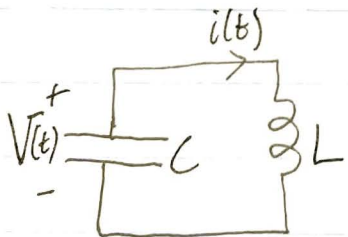
8.  $> 0$ : The current will grow towards  $+\infty$   
 $< 0$ : The current will tend to  $-\infty$   
 $= 0$ : The current will be bounded
- Inductors  
INTEGRATE  
Voltage

9. For a given two-terminal linear circuit, the circuit transfers power to some resistive load. This power is maximized when the load has resistance  $R_{TH}$ , the Thevenin resistance of the circuit. This maximized power is given by  $V_{TH}^2 / 4R_{TH}$

10.

	Pro	Con
overdamped	No oscillations	Slowest decay
critically	fastest decay	unrealizable
underdamped	faster decay than overdamped, realizable	oscillatory response

11.



$$L \frac{di}{dt} + \frac{1}{C} \int i(t) dt = 0 \quad ] \text{KVL}$$

$$L \frac{d^2 i}{dt^2} + \frac{1}{C} i(t) = 0 \quad ] \frac{d}{dt} \text{ both sides}$$

so Eqn:  $\frac{d^2 i}{dt^2} + \frac{1}{LC} i(t) = 0$

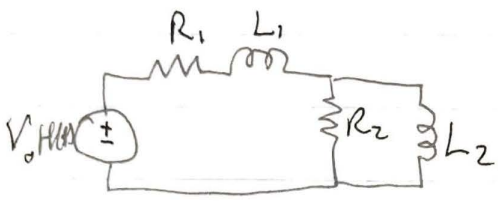
char. eqn:  $m^2 + \frac{1}{LC} = 0 \Rightarrow m = \pm j \frac{1}{\sqrt{LC}}, \omega = \frac{1}{\sqrt{LC}}$ , response

from  $V_0 = V_0$

$A \cos \omega t + B \sin \omega t = i(t)$ , A, B not both zero as there is

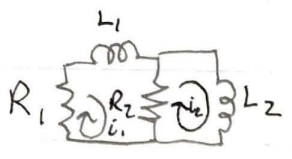
energy initially in the system. Theoretically it does go forever. Realistically, there will be some parasitic resistance to cause damping.

12.



For transient, can turn off source

Mesh:



~~$(i_1 - i_2)R_2 + i_1 R_1 + L_1 \frac{di_1}{dt} = 0$~~

①  $(i_1 - i_2)R_2 + i_1 R_1 + L_1 \frac{di_1}{dt} = 0$

②  $L_2 \frac{di_2}{dt} + (i_2 - i_1)R_2 = 0$

From ②,  $i_1 = \frac{L_2}{R_2} \frac{di_2}{dt} + i_2$ . Plug into ①:

$$\left( \frac{L_2}{R_2} \frac{di_2}{dt} + i_2 - i_2 \right) R_2 + \left( \frac{L_2}{R_2} \frac{di_2}{dt} + i_2 \right) R_1 + L_1 \frac{d}{dt} \left( \frac{L_2}{R_2} \frac{di_2}{dt} + i_2 \right) = 0$$

↓

$$\frac{L_1 L_2}{R_2} \frac{d^2 i_2}{dt^2} + \left( \frac{L_2 R_1}{R_2} + L_2 + L_1 \right) \frac{di_2}{dt} + R_1 i_2 = 0$$

↓

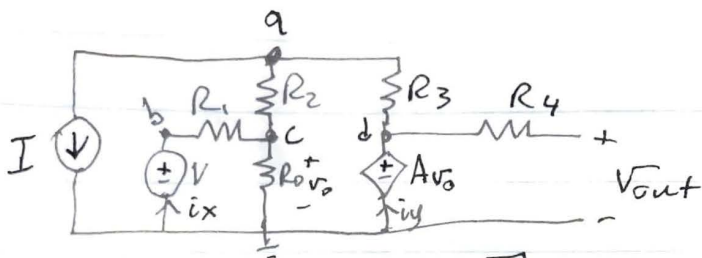
$$a \frac{d^2 i_2}{dt^2} + b \frac{di_2}{dt} + c i_2 = 0, \quad \alpha = \frac{b}{2a}, \quad \omega = \sqrt{\frac{c}{a}}$$

overdamped:  $\alpha > \omega$

underdamped:  $\alpha < \omega$

Critically damped:  $\alpha = \omega$

13.



$V_{TH}$ :  $v_d = V_{TH}$ ,  $v_o = v_c$  } solve system,  $v_d$  will give  $V_{TH}$

$t_1$ :  $v_b = V$

$t_2$ :  $A v_c = v_d$

a:  $I + (v_a - v_c)G_2 + (v_a - v_d)G_3 = 0$

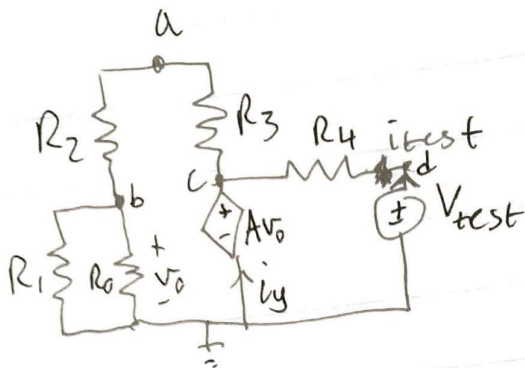
b:  $i_x + (v_c - v_b)G_1 = 0$

c:  $(v_b - v_c)G_1 + (v_a - v_c)G_2 = (v_c)G_o$

d:  $i_y + (v_a - v_d)G_3 = 0$

$$\begin{pmatrix} G_2 + G_3 & 0 & -G_2 & -G_3 & 0 & 0 \\ 0 & -G_1 & G_1 & 0 & 1 & 0 \\ G_2 & G_1 & -G_o - G_1 - G_2 & 0 & 0 & 0 \\ G_3 & 0 & 0 & -G_3 & 0 & 1 \\ 0 & 1 & 0 & 0 & 0 & 0 \\ 0 & 0 & A & -1 & 0 & 0 \end{pmatrix} \begin{pmatrix} v_a \\ v_b \\ v_c \\ v_d \\ i_x \\ i_y \end{pmatrix} = \begin{pmatrix} -I \\ 0 \\ 0 \\ 0 \\ V \\ 0 \end{pmatrix}$$

For  $R_{TH}$ :



$$v_a = v_b$$

Solve system,  $\frac{V_{test}}{i_{test}} = R_{TH}$

$$t_1: Av_b = v_c$$

$$t_2: v_d = V_{test}$$

$$a: (v_a - v_b)G_2 + (v_a - v_c)G_3 = 0$$

$$b: (v_b - v_a)G_2 + v_b G_1 + v_b G_0 = 0$$

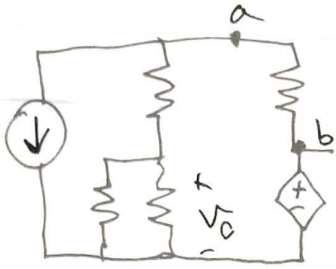
$$c: i_y + (v_a - v_c)G_3 + (v_d - v_c)G_4 = 0$$

$$d: i_{test} + (v_c - v_d)G_4 = 0$$

$$\begin{pmatrix} G_2 + G_3 & -G_2 & -G_3 & 0 & 0 & 0 \\ -G_2 & G_0 + G_1 + G_2 & 0 & 0 & 0 & 0 \\ G_3 & 0 & -G_3 - G_4 & G_4 & 1 & 0 \\ 0 & 0 & G_4 & -G_4 & 0 & 1 \\ 0 & A & -1 & 0 & 0 & 0 \\ 0 & 0 & 0 & 1 & 0 & 0 \end{pmatrix} \begin{pmatrix} v_a \\ v_b \\ v_c \\ v_d \\ i_y \\ i_{test} \end{pmatrix} = \begin{pmatrix} 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ V_{test} \end{pmatrix}$$

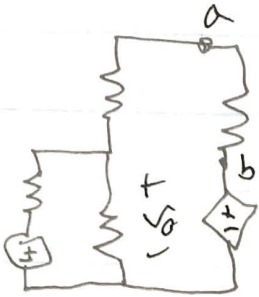
14.

①



and

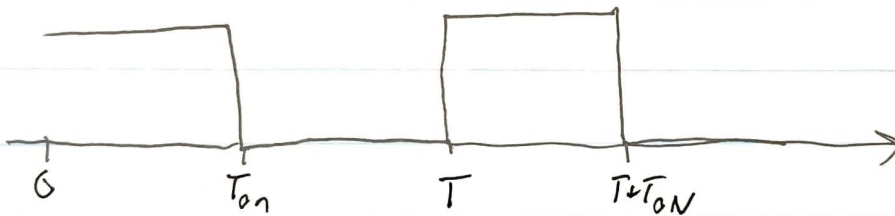
②



$$V_1 = V_a - V_b \text{ for ckt 1 with MNA}$$

$$V_2 = V_a - V_b \text{ for ckt 2 with MNA}$$

$$V_1 + V_2 = V_{\text{total}}$$

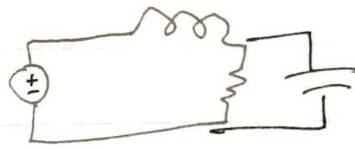
15.  $\frac{V}{R}$ 

$$16. \quad P = \frac{1}{T} \int_0^T v(t) i(t) dt = \frac{1}{T} \int_0^{T_{on}} V \left( \frac{V}{R} \right) dt + \frac{1}{T} \int 0 dt$$

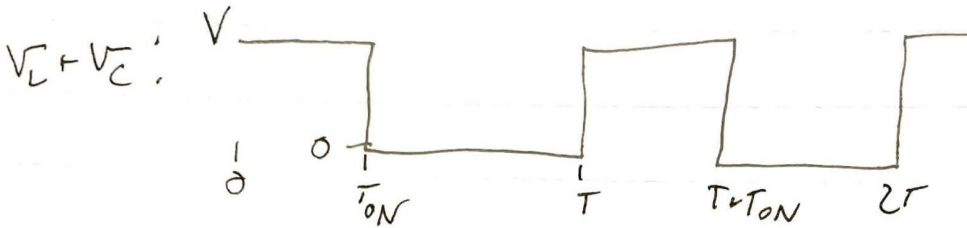
$$= \frac{T_{on}}{T} \frac{V^2}{R} = D \frac{V^2}{R}$$

if switch always closed, power is  $\frac{V^2}{R}$ , so factor of  $D$  difference ( $D < 1$  so less)

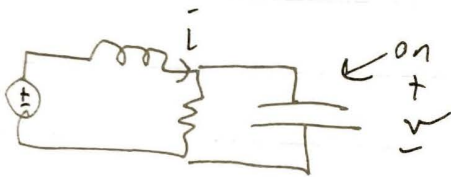
17,  $0 \rightarrow T_{ON}: V_L + V_C = V$



$T_{ON} \rightarrow T: V_L + V_C = 0$



18.



$i_{SS_{off}} = 0$   
 $V_{SS_{off}} = 0$

$i_{SS_{on}} = V/R$

$V(T_{ON}^-) = V(T_{ON}^+)$

$V(0) = V(T)$

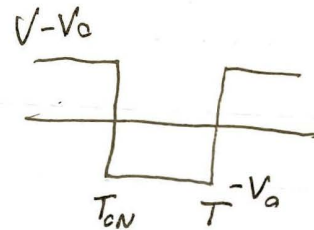
$V_{SS_{on}} = V$

$i(T_{ON}^-) = i(T_{ON}^+)$

$i(0) = i(T)$

i.e. final conds. of on ckt are initial conds. of off ckt.

19.  $V_L = \begin{cases} V - V_0, & 0 < t < T_{ON} \\ -V_0, & T_{ON} < t < T \end{cases}$



$L \frac{di}{dt} = V_L(t)$

$i(t) = \frac{1}{L} \int V_L(t) dt = \begin{cases} \frac{1}{L}(V - V_0)t + C_0, & 0 < t < T_{ON} \\ \frac{1}{L}(-V_0)t + C_1, & T_{ON} < t < T \end{cases}$

$C_0 = I_0$ ,  ~~$I_{MAX}$~~



$\frac{1}{L}(V - V_0)T_{ON} + I_0 = \frac{1}{L}(-V_0)T_{ON} + C_1 \Rightarrow C_1 = I_0 + \frac{T_{ON}V}{L}$

↑  
you need not actually do this to solve!



$$20. \Delta \bar{i}_{ON} = \left( \frac{1}{L} (V - V_o) T_{ON} + I_o - \bar{I}_o \right) = \frac{1}{L} (V - V_o) \bar{T}_{ON}$$

~~$$\Delta \bar{i}_{OFF} = \left( \frac{1}{L} (V - V_o) T_{ON} + I_o - \bar{I}_o \right)$$~~

$$\Delta \bar{i}_{OFF} = \left( \frac{1}{L} (V - V_o) T_{ON} + I_o - \frac{1}{L} (-V_o) T - \bar{I}_o - \frac{T_{ON} V}{L} \right)$$

$$= - \left( -\frac{V_o}{L} T_{ON} + \frac{V_o}{L} T \right) = \frac{V_o}{L} (T_{ON} - T)$$

$$\Delta \bar{i}_{CN} = -\Delta \bar{i}_{OFF}$$

$$21. \frac{V_o}{L} (T_{ON} - T) = -\frac{1}{L} (V - V_c) T_{ON}$$

$$\Rightarrow V_o (T_{ON} - T) = V_o T_{ON} - V T_{ON}$$

$$\Rightarrow -V_o T = -V T_{ON}$$

$$\Rightarrow \frac{V_o}{V} = \frac{T_{ON}}{T} = D$$

22. C large, for example